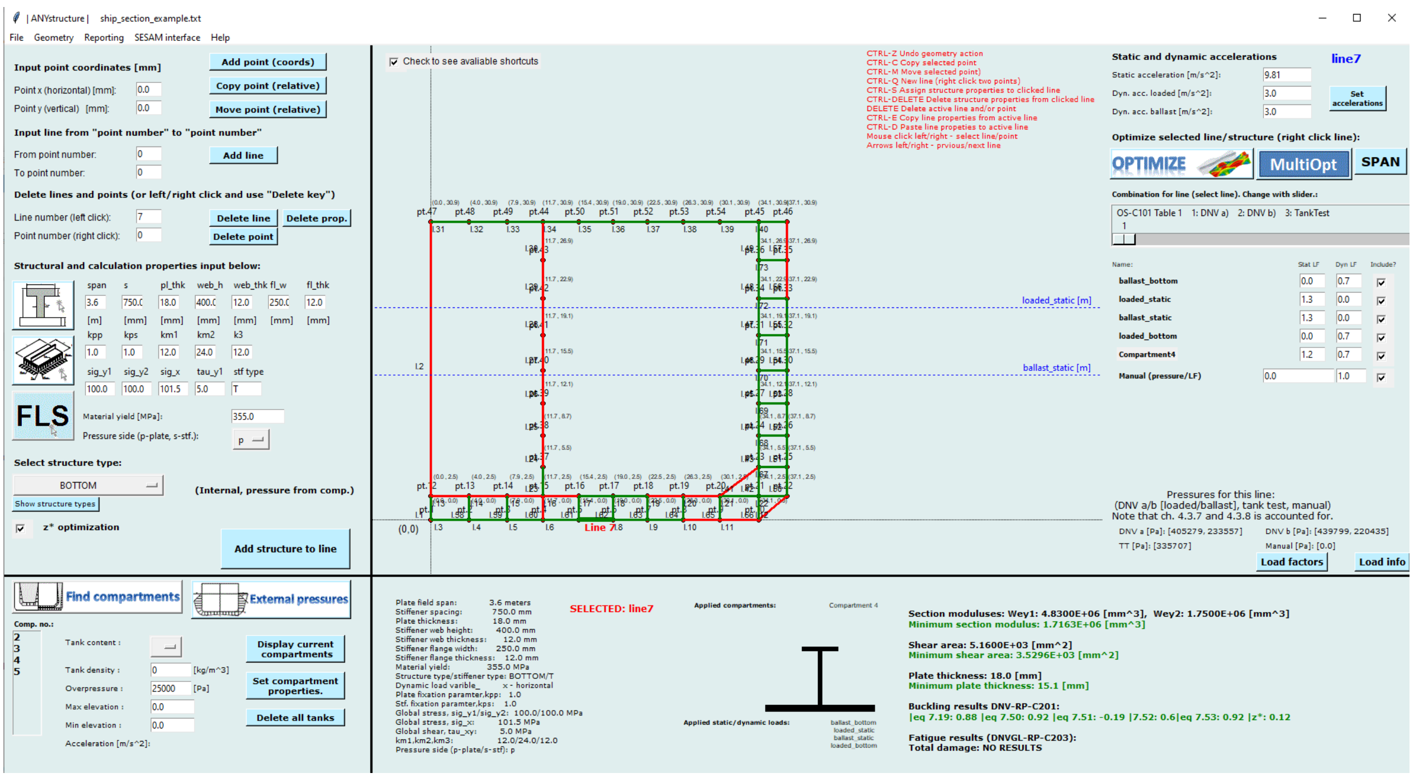
ANYstructure



Documentation

2021

Version 2.X

Table of contents

Theory

All calculations are according to the following DNVGL standards and recommended practices:

- **DNVGL-OS-C101 Design of offshore steel structures, general - LRFD method**
    - **http://rules.dnvgl.com/docs/pdf/DNVGL/OS/2018-07/DNVGL-OS-C101.pdf**
- **DNV-RP-C203 Fatigue design of offshore steel structures**
- **DNV-RP-C201 BUCKLING STRENGTH OF PLATED STRUCTURES**
    - **https://rules.dnvgl.com/docs/pdf/DNV/codes/docs/2010-10/RP-C201.pdf**

Modelling

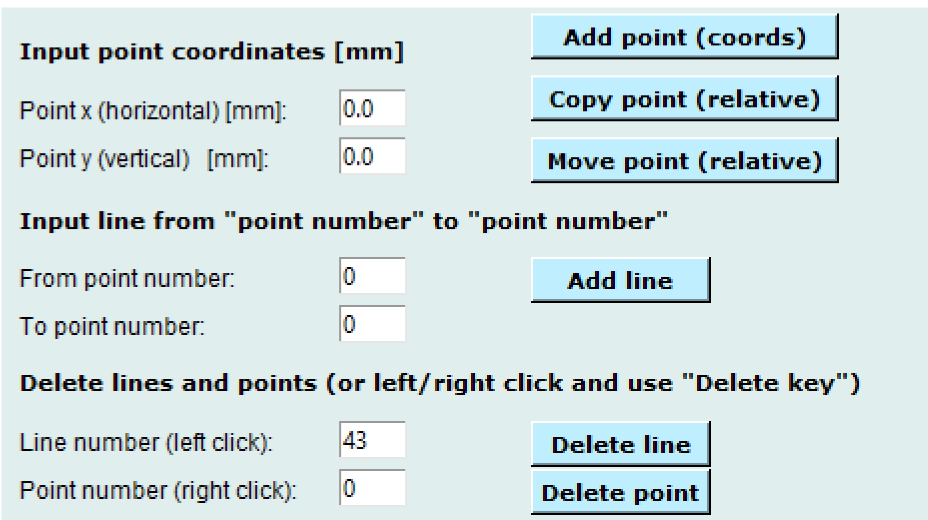
Modelling is done in upper left corner.

Right click: **select point**

You can copy or move the selected point by shortcut or clicking Buttons.

Left click: **select line**

A line is made by right clicking two points (or input point number)



Speed up your modelling significantly by using the shortcuts:

CTRL-Z	**Undo modelling**
CTRL-P	**Copy a selected point**
CTRL-M	**Move a selected point**
CTRL-Q	**New line between two selected points**
CTRL-S	**Assign properties to a selected line**
CTRL-DELETE	**Delete the structural properties from the selected line**

DELETE **Delete selected line/point**

CTRL-E **Select a line and copy the properties of this line**

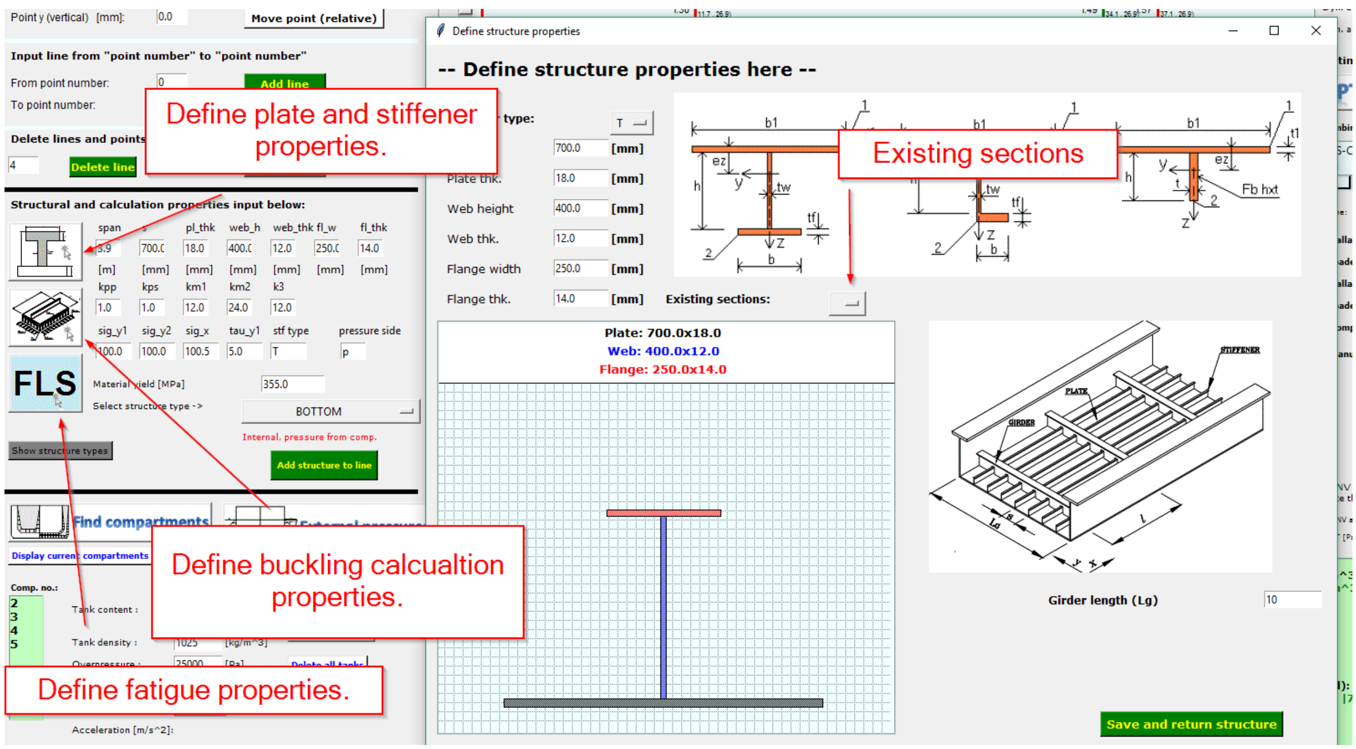
CTRL-D **Paste structural properties to a selected line**

Left and right arrow to change current line.

Assigning properties

Input properties manually or click the button indicated below to set the values. Values are set by clicking "Add structure to line". This also applies to fatigue properties. If you have added a property to a line and want to use the same for the next line, just press "Add structure to line" on the new line.

All beam sections are recorded. If you want to apply an existing, choose it from the drop down menu. Then press "Save and return structure".

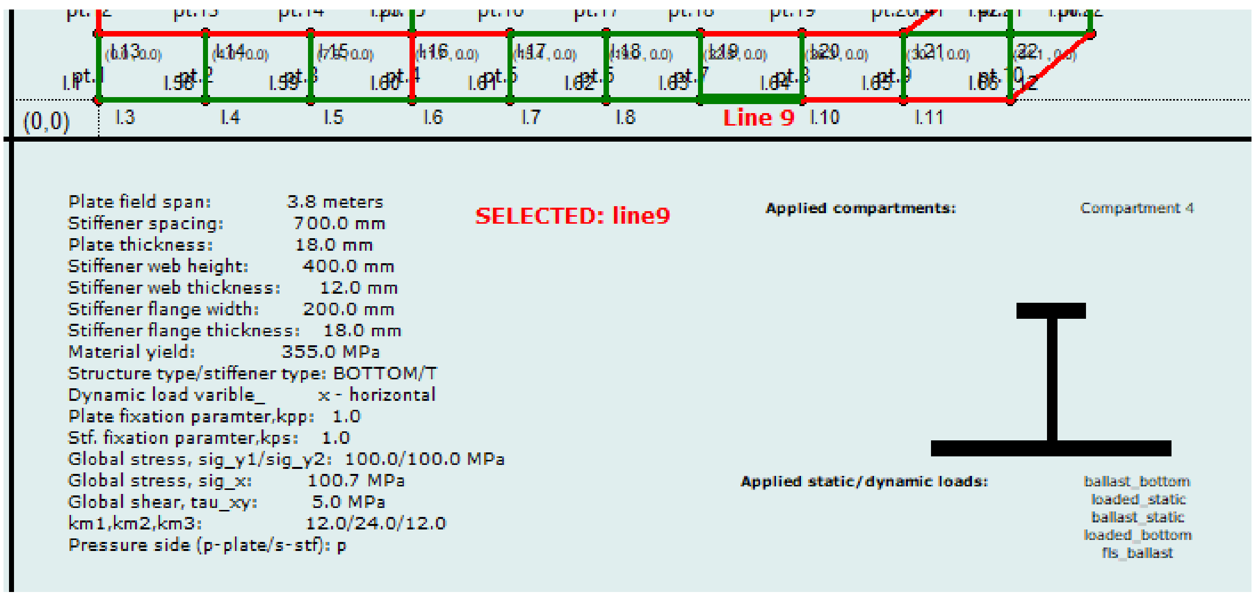


By default z* is ticked. This affects the buckling results and will generally give lower utilization than using z* = 0. See description below.

z^* is the distance from the neutral axis of the effective section to the working point of the axial force. z^* may be varied in order to optimise the resistance. z^* should then be selected so the maximum utilisation found from the equations (7.50) to (7.53) or (7.54) to (7.57) is at its minimum, see also Commentary Chapter 10. The value of z^* is taken positive towards the plate. The simplification $z^* = 0$ is always allowed.

Display properties

If you click a line properties is displayed in the window below as seen next.

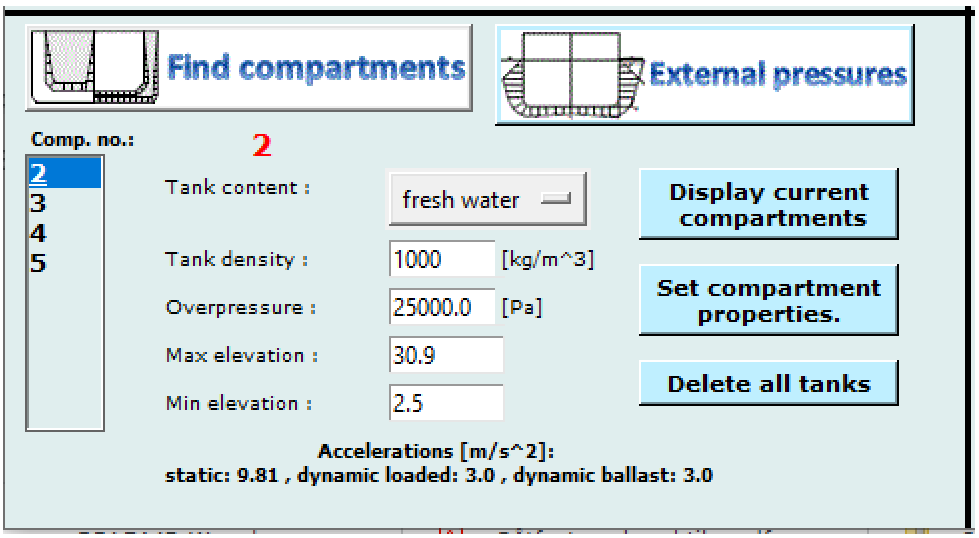


Define tanks

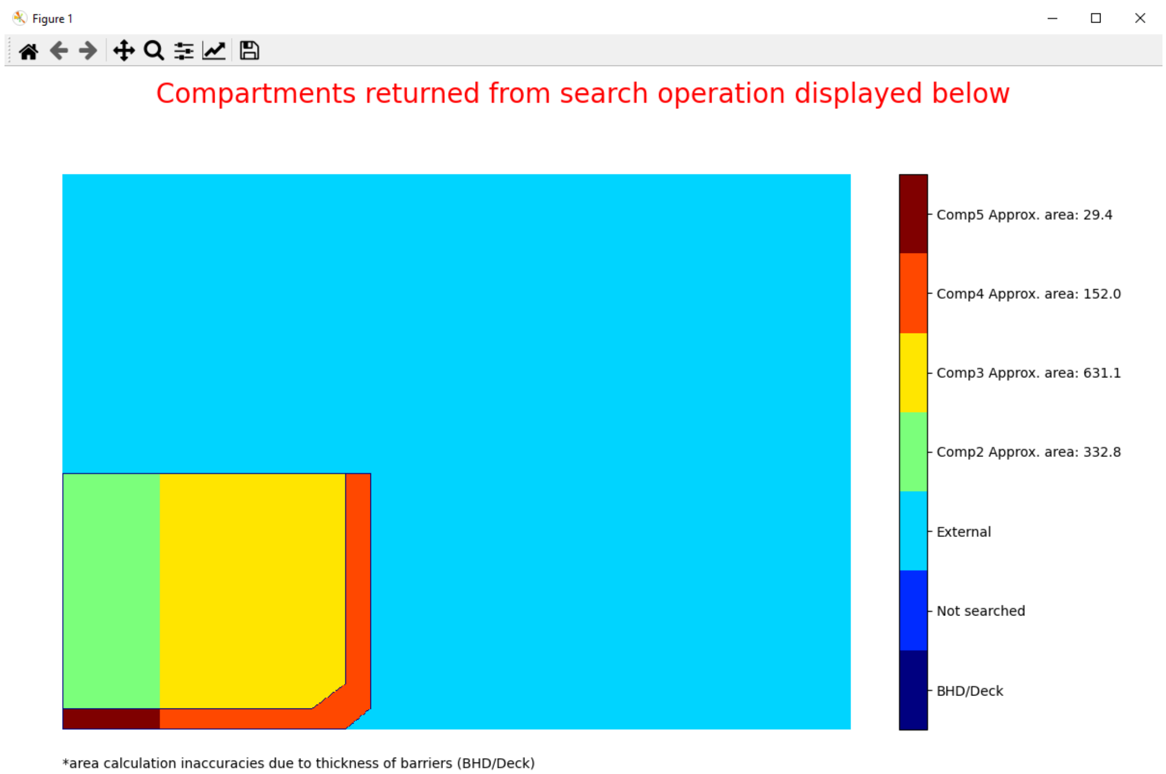
Tanks are searched for when clicking “Find compartments”. Non watertight structure are ignored. For information on structure types click “Show structure types”.

By default tank content density is set to 0.

Ather tanks are found content and overpressure must be defined as seen next.

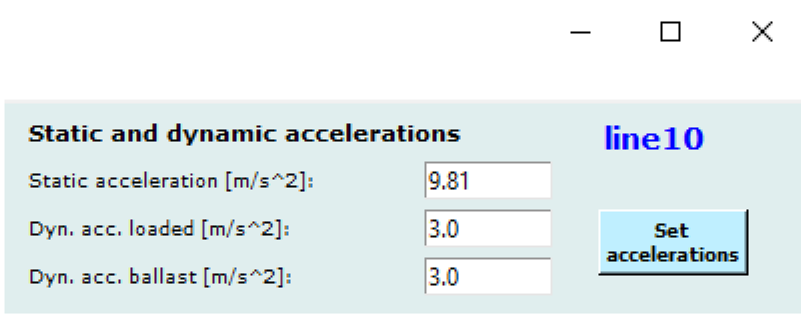


If you press “Display current compartments” after doing a compartment search, the result of the search is illustrated as seen next. Approximate area of the respective compartments is also shown.



Setting accelerations

Accelerations applies to tank content. I is set in the upper right corner as seen next.



Define external pressures

Click “External pressures” to define pressures acting on the structures.

NOTE:

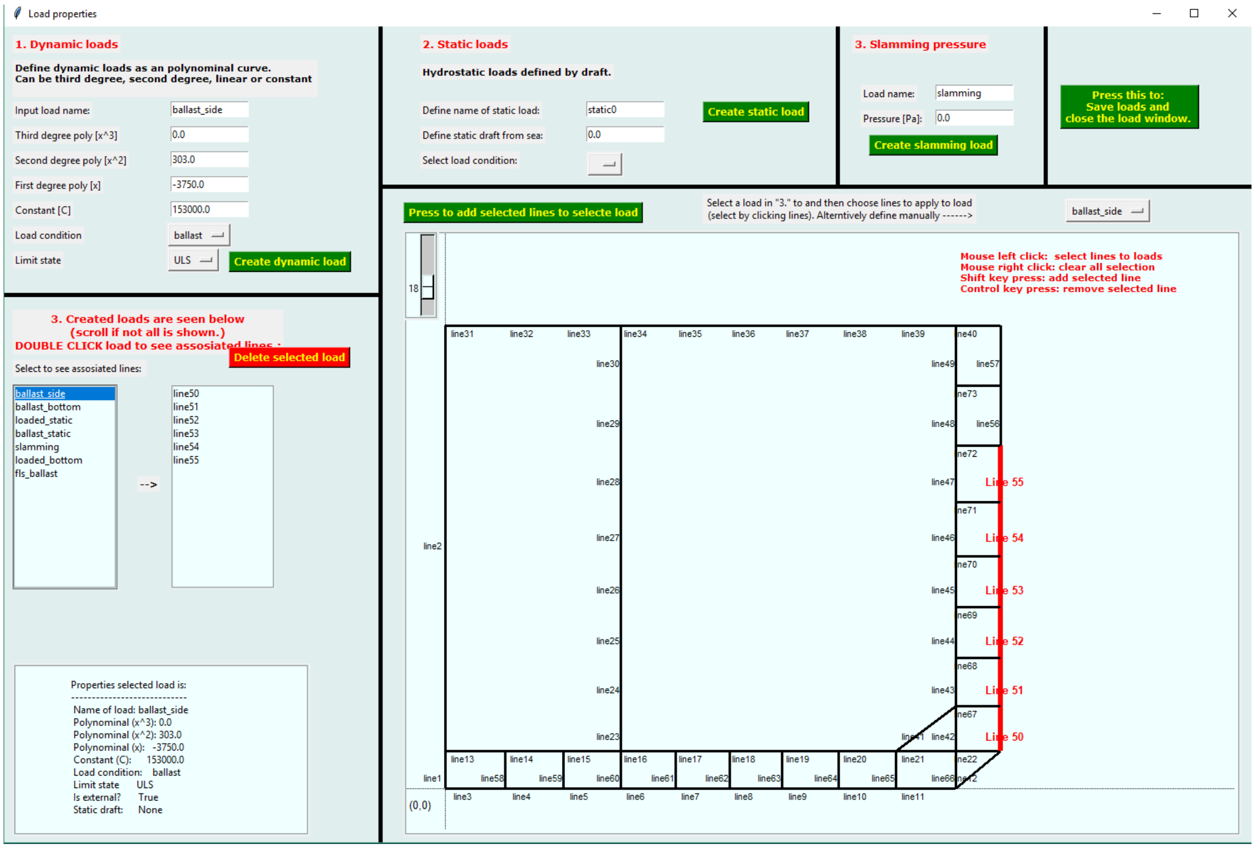
FOR DYNAMIC EQUATION THE FOLLOWING APPLIES

X (horizontal) used for BOTTOM, BBT, HOPPER, MD

Z (vertical) used for BBS, SIDE_SHELL, SSS

After new window is opened:

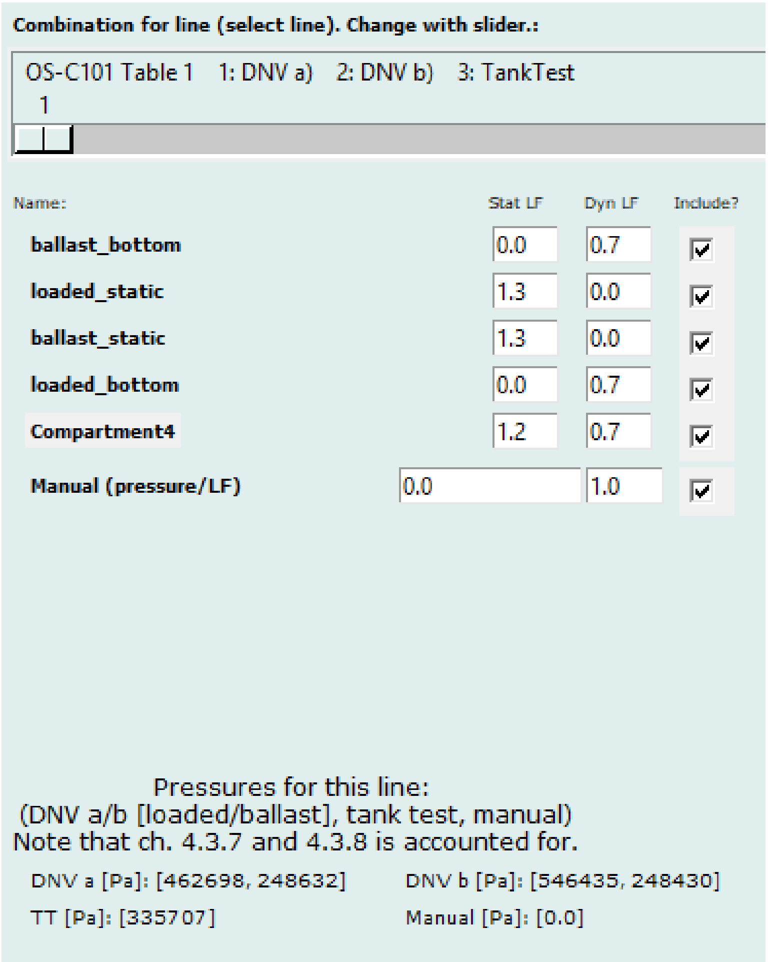
1. **Make dynamic loads**
    a. **Dynamic loads are made by defining up to 3rd degree equations. X or Y direction depends on the defined structure type.**
    b. **Note that you can define a constant dynamic load by using Constant (Constant (C)) only.**
2. **Static loads are calculated according to depth.**
3. **To apply a defined load to a line or multiple lines:**
    a. **a. Select load by clicking the created load**
4. **Click the lines that shall have the load. Click the button “Press to add selected lines to selected load”**
5. **When finished press the button in the upper right corner.**



Load combinations

Load combinations are created automatically after external pressures are defined. Some comments on the loads.

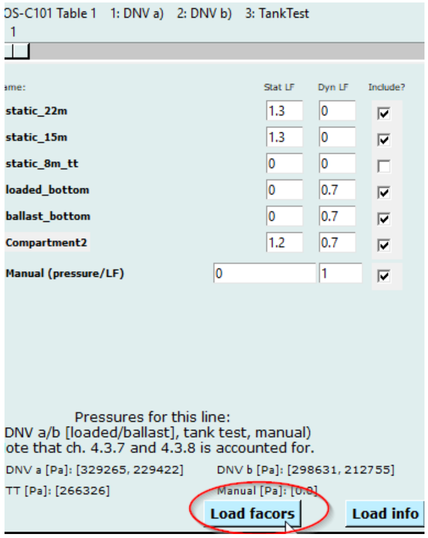
1. **According to DNVGL-OS-C101**
2. **Highest pressure are chosen w.r.t. tank filling.**
3. **You can deselect a load by manually inputting load factor to 0 or deselect include.**

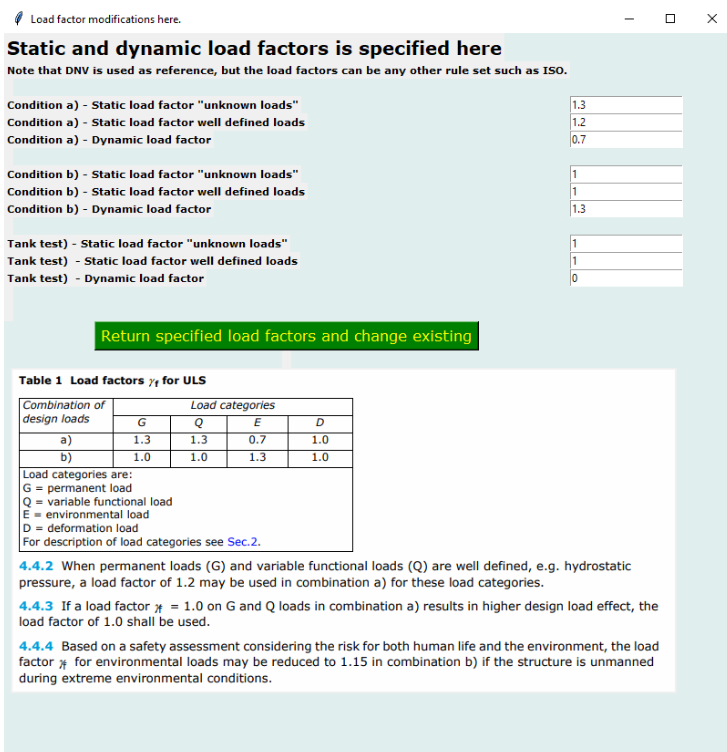


Changing load factors

You can change default load factors and existing load factors using the button seen in the next illustration.

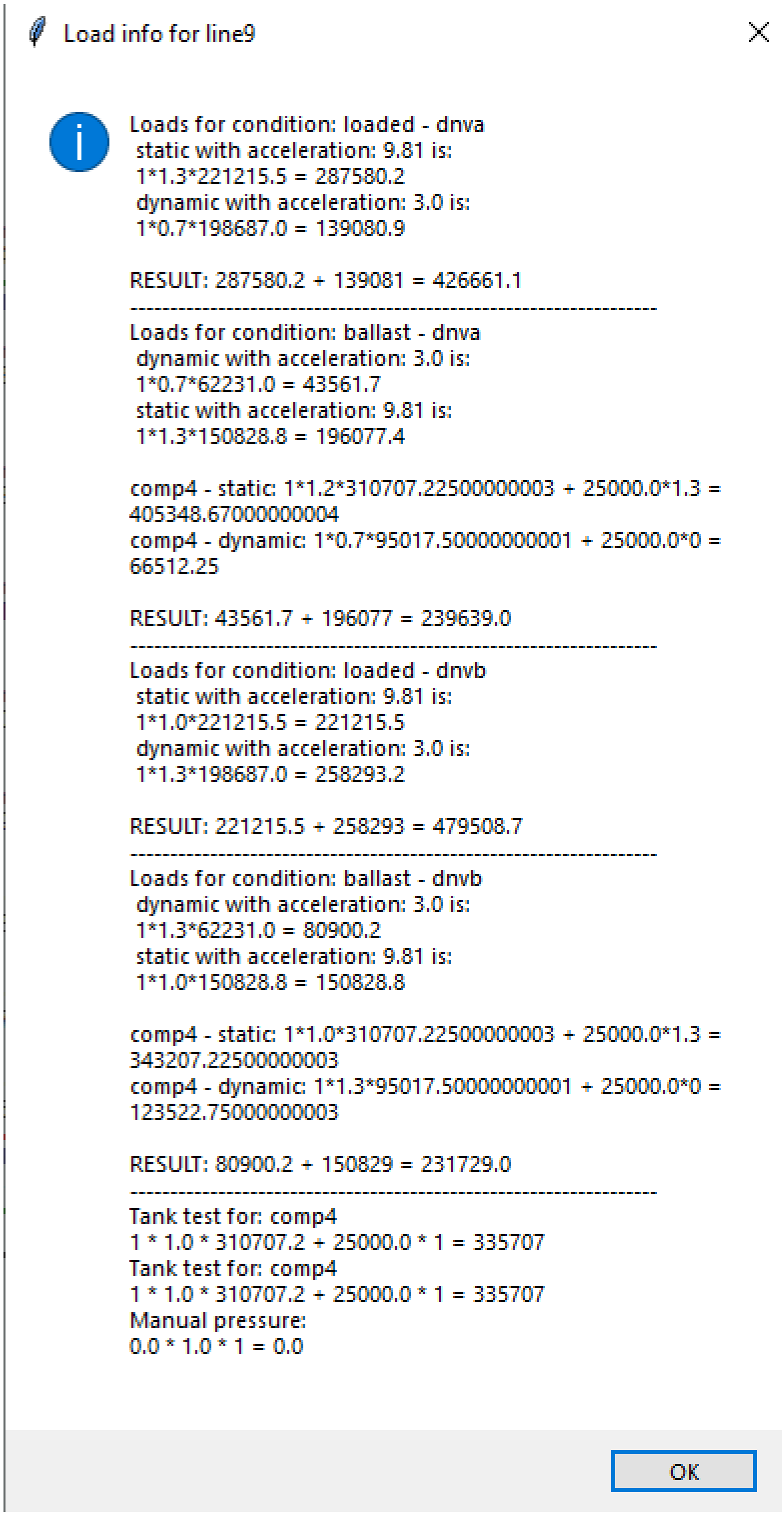
Load factors are based on standard DNV LRFD factors, but any values can be used.





Reviewing loads

Load calculations and results can be reviewed by clicking the “Load info” button. An example is seen in the next illustration.


Load info for line9
Loads for condition: loaded - dnva
static with acceleration: 9.81 is:
1*1.3*221215.5 = 287580.2
dynamic with acceleration: 3.0 is:
1*0.7*198687.0 = 139080.9
RESULT: 287580.2 + 139081 = 426661.1

Loads for condition: ballast - dnva
dynamic with acceleration: 3.0 is:
1*0.7*62231.0 = 43561.7
static with acceleration: 9.81 is:
1*1.3*150828.8 = 196077.4
comp4 - static: 1*1.2*310707.22500000003 + 25000.0*1.3 = 405348.67000000004
comp4 - dynamic: 1*0.7*95017.50000000001 + 25000.0*0 = 66512.25
RESULT: 43561.7 + 196077 = 239639.0

Loads for condition: loaded - dnvb
static with acceleration: 9.81 is:
1*1.0*221215.5 = 221215.5
dynamic with acceleration: 3.0 is:
1*1.3*198687.0 = 258293.2
RESULT: 221215.5 + 258293 = 479508.7

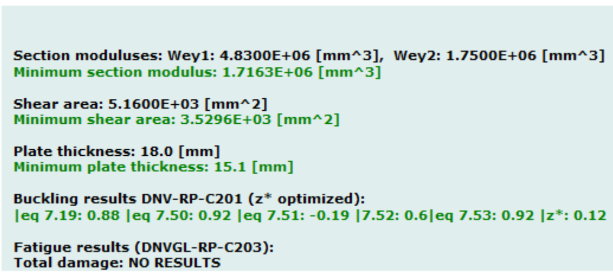
Loads for condition: ballast - dnvb
dynamic with acceleration: 3.0 is:
1*1.3*62231.0 = 80900.2
static with acceleration: 9.81 is:
1*1.0*150828.8 = 150828.8
comp4 - static: 1*1.0*310707.22500000003 + 25000.0*1.3 = 343207.22500000003
comp4 - dynamic: 1*1.3*95017.50000000001 + 25000.0*0 = 123522.75000000003
RESULT: 80900.2 + 150829 = 231729.0

Tank test for: comp4
1 * 1.0 * 310707.2 + 25000.0 * 1 = 335707
Tank test for: comp4
1 * 1.0 * 310707.2 + 25000.0 * 1 = 335707
Manual pressure:
0.0 * 1.0 * 1 = 0.0
OK

Results

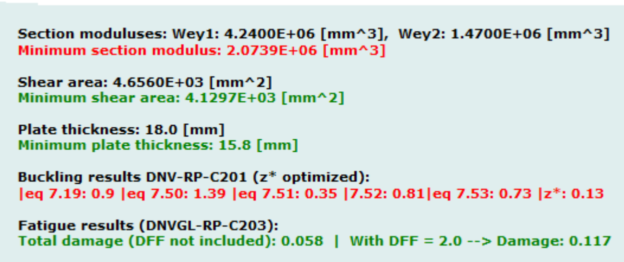
When clicking a line, results as presented in the window below. If the result for the clicked line is OK, the color of the line and text is green. If the result is NOT OK, the color of the line and text is red. Two examples are seen next.

All results ok



Section modulus not ok

Buckling not ok

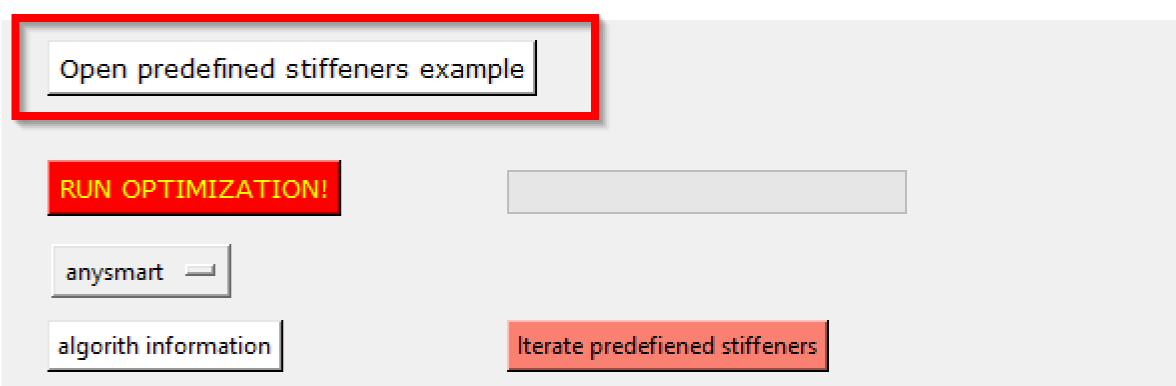


Optimization

Optimization iteration by predefined stiffeners

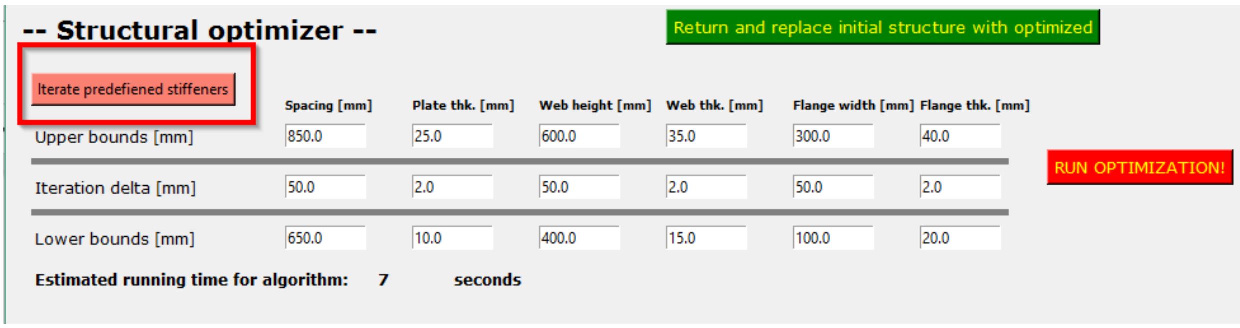
From 0.5 you can iterate by a defined set of stiffeners. Press the button marked below. Open a csv (or json) file. Then start your iterations. The only other input is the stiffener spacing and plate thickness.

To see how the input format is click the "open predefined stiffeners example" button. See illustrations next.



Note that the weight of your initial structure is ignored even though it is calculated. If the initial structure is in your predefined set it will be included in the evaluations.

Press the button indicated below to activate. A open file window will open when running the optimization.



Single optimization

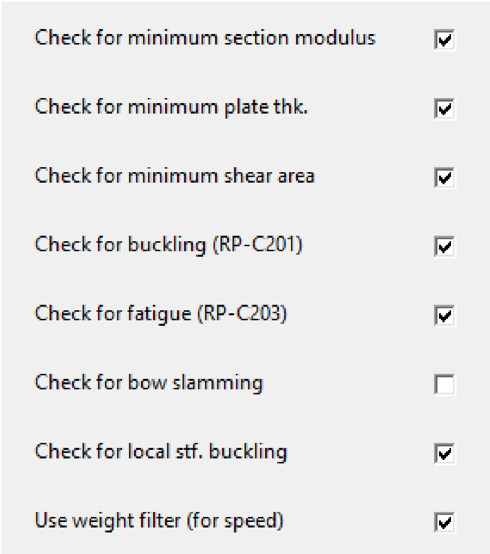
Single optimization is done by clicking a line and clicking the "OPTIMIZE" button.

1. **Set the upper and lower bounds of the optimization.**
2. **Set the delta to be used for the searched. This is the step size of the optimization when using brute force method (for example anysmart).**
3. **Run the optimization.**
4. **If you are happy, return the properties by clicking the top button**

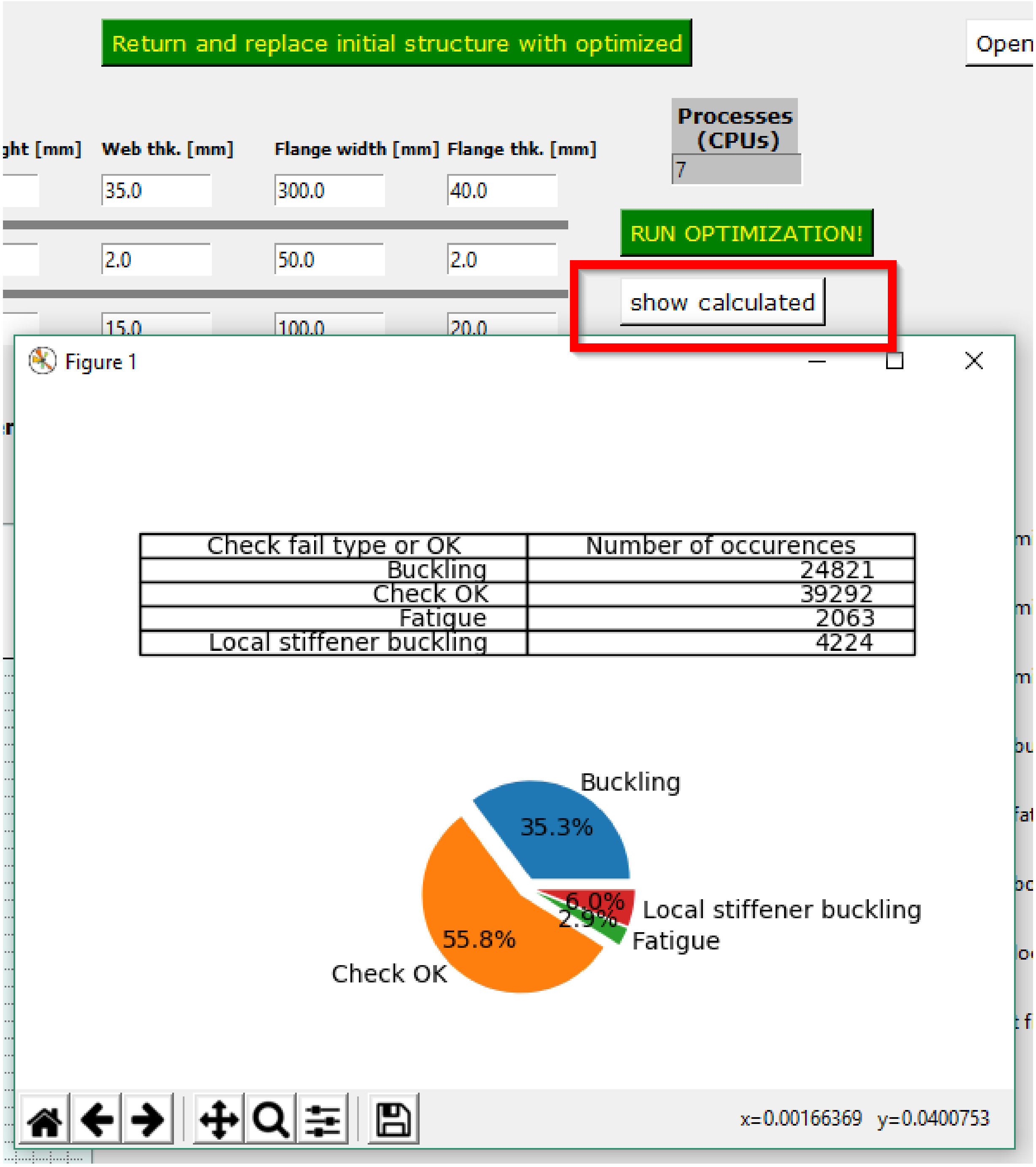
Various checks in the optimization module:

You can select the checks to be performed.

The weight filter ensures that only sections with a lower weight than the current minimum weight. This significantly speed up the calculations, but if you want to see the full distribution of the various checks this must be unchecked.

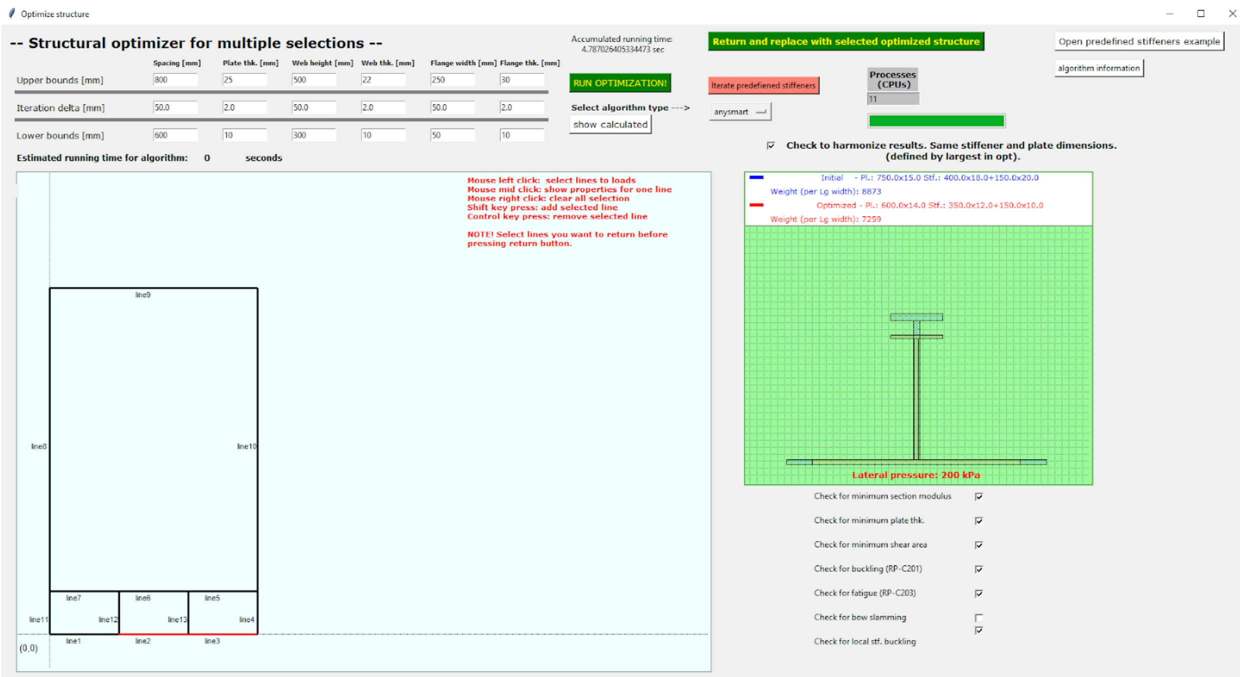


If you press the “show calculated” button, you will get an overview of how many is ok and how many failed (and what criteria first failed). One “occurence” is a one checked plate/stiffener combination.



You will also be asked to save to a csv file. If you do not cancel, a csv file will ALL results will pre saved to your chosen location. If you open the file in excel you should see something like show next

Multiple optimization



Multiple optimization is done by clicking the "MultiOpt" button.

1. **Same input on upper bounds, lower bounds and delta.**
2. **Click all the lines you want to include in the optimization.**
3. **Run the optimization.**
4. **Check the properties by middle clicking the line you ran.**
5. **If you are happy return the properties by clicking the top button. Remember to select the lines you want to return. Lines that have been optimized is marked orange.**

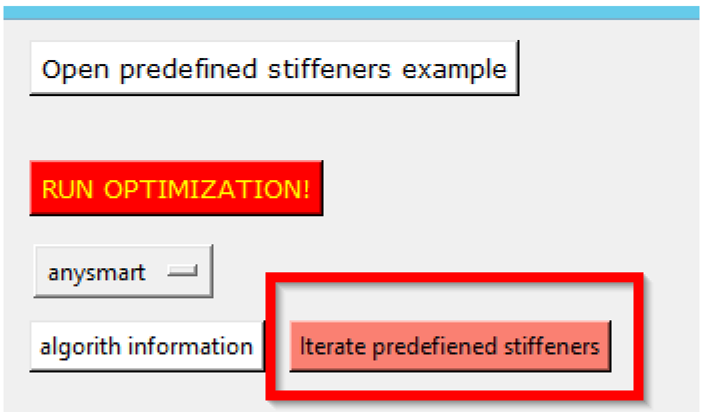
The optimization can be harmonized. That means that the larges dimension found in the multiple optimization is used for all selected. This is done after all plates/stiffeners are checked. Harmonization can only be done in the multiopt option

Other options that can be set is explained in the single optimization chapter.

When showing calculated you must have selected a line (middle click).

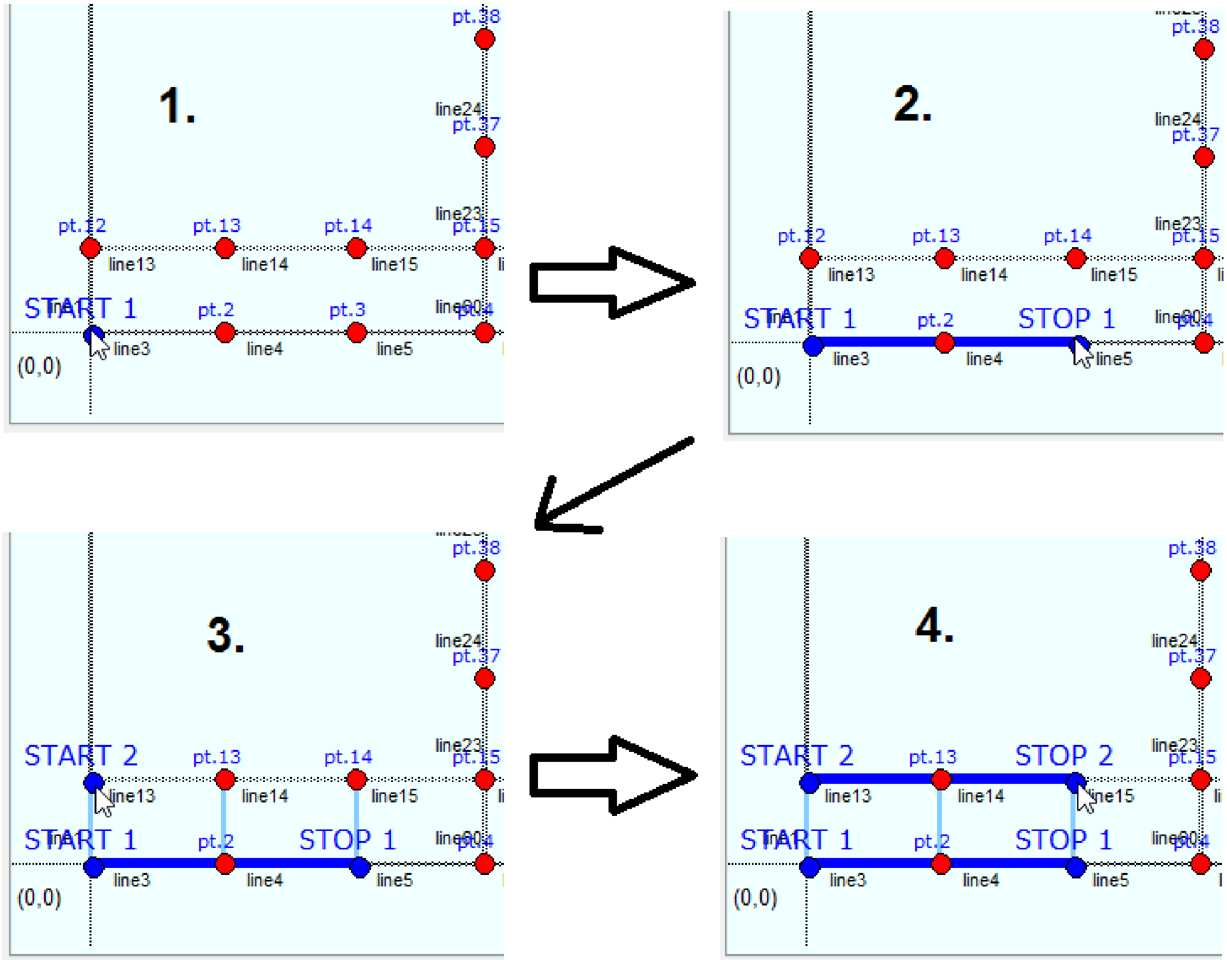
Span optimization

NOTE: The span optimization is computationally heavy. It is recommended to use a set of predefined stiffeners.



The optimization is started as follows.

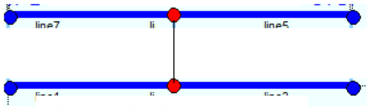
1. **Start by clicking as illustrated next:**



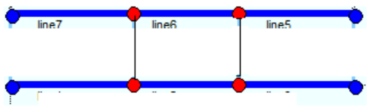
2. Then run optimization.

The program will calculate variations of even spans in your structure as illustrated next. This is an example and number of plate fields may vary.

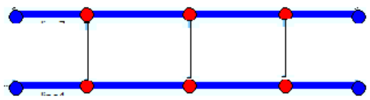
4 plate fields



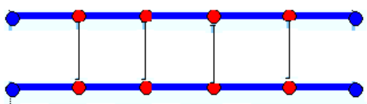
6 plate fields



8 plate fields



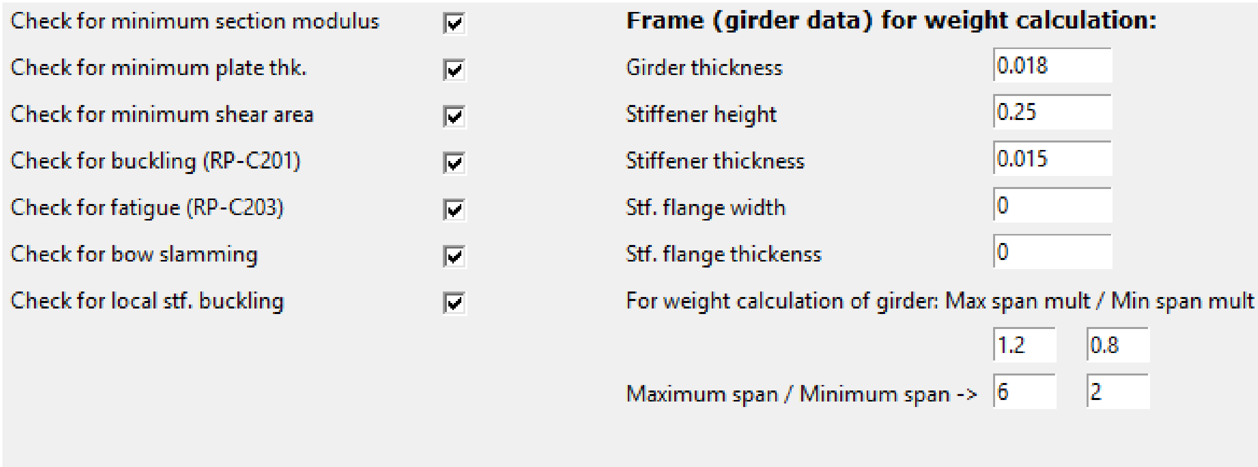
10 plate fields



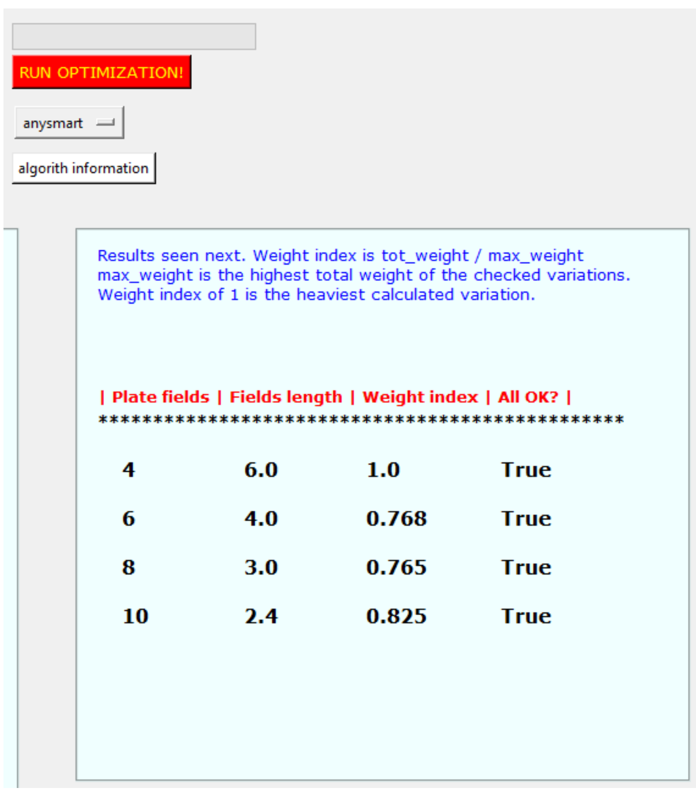
You can, similar to single optimization, select the checks that shall be runned. Also you can set the girder (frame) properties. This is used for calculating the weights.

With reference to the example above, max span mult is the multiplicator for the 4 plate fields set up and min span mult is the weight multiplication for the 10 plate field set up. This is adopted because one can assume the required dimensions for the girder will reduce when more girders are added.

Minimum span and maximum span is the minimum and maximum span of the plate fields in meters.

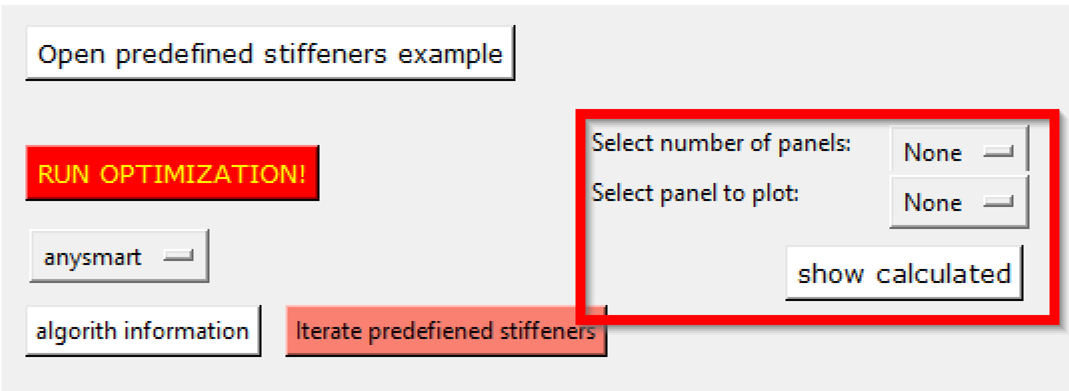


Results are presented as seen next.



In this case 8 plate fields with length of 3 meter will give the lowest weight. 6 plate fields is almost equal.

When the analysis has been runned you should save your results. Just specify a file name in the save file dialog. You can also get detailed individual results for a specified panel. Select number of plate fields in the iteration you want to look at, then choose which panel to get data from. Order of the panels is the same as printed in the left result canvas.



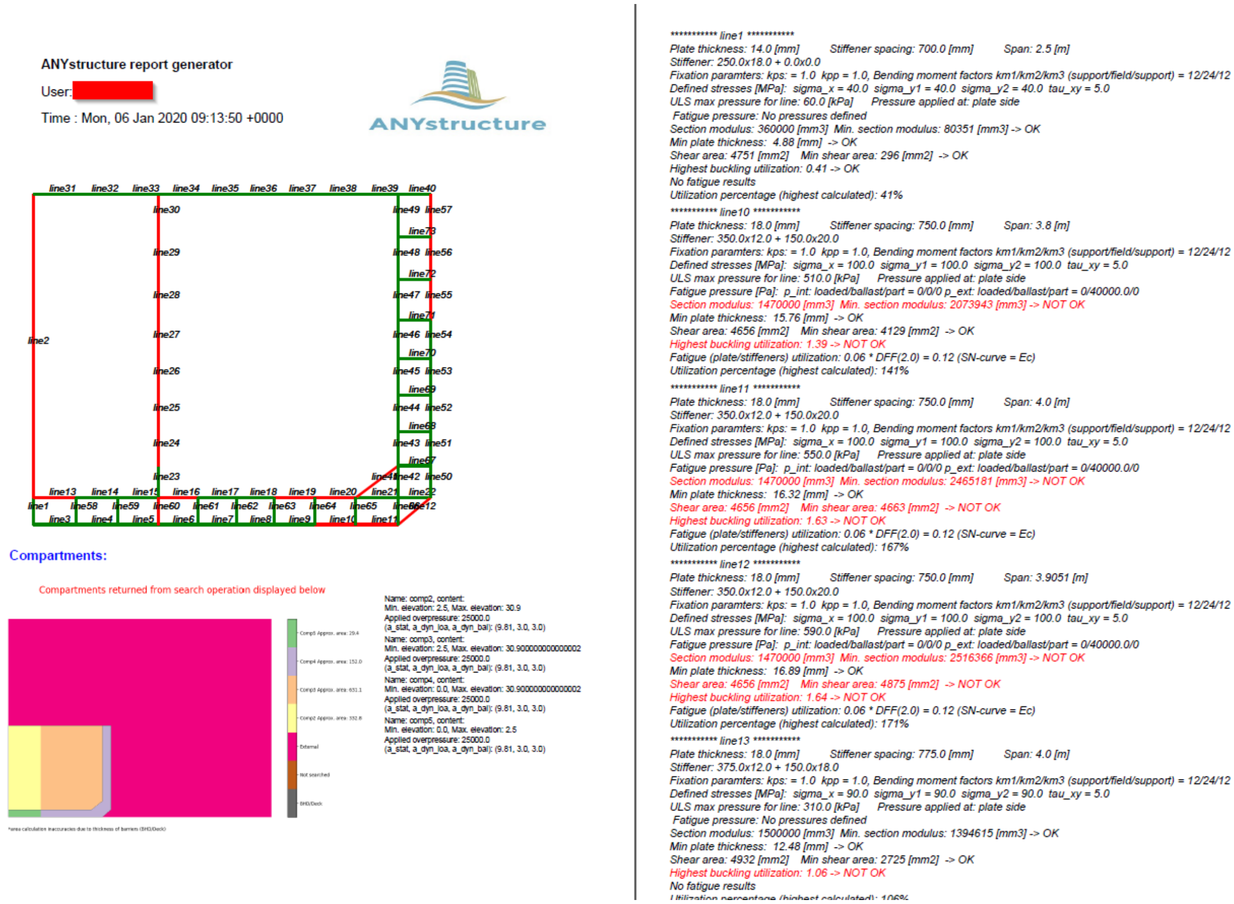
Now close the window. Results are not currently returned to main window.

Detailed results, printed after running, looks like this :

```
------------------------------------------------------------------------
Plate fields: 22 Frames: 10
pl_650.0x14.0 stf_L180.0x8.0+33.0x17.8 span: 1.0636 structure type: BOTTOM stf. type: L pressure side: p | sigma_y1: 128.6 sigma_y2: 128.6 sigma_x: 177.9 tauxy: 6.4 START 1 OK!
pl_650.0x14.0 stf_L180.0x8.0+33.0x17.8 span: 1.0636 structure type: BOTTOM stf. type: L pressure side: p | sigma_y1: 128.6 sigma_y2: 128.6 sigma_x: 177.9 tauxy: 6.4 ------- OK!
pl_650.0x14.0 stf_L180.0x8.0+33.0x17.8 span: 1.0636 structure type: BOTTOM stf. type: L pressure side: p | sigma_y1: 128.6 sigma_y2: 128.6 sigma_x: 177.9 tauxy: 6.4 ------- OK!
pl_650.0x14.0 stf_L180.0x8.0+33.0x17.8 span: 1.0636 structure type: BOTTOM stf. type: L pressure side: p | sigma_y1: 128.6 sigma_y2: 128.6 sigma_x: 177.9 tauxy: 6.4 ------- OK!
pl_650.0x14.0 stf_L180.0x8.0+33.0x17.8 span: 1.0636 structure type: BOTTOM stf. type: L pressure side: p | sigma_y1: 128.6 sigma_y2: 128.6 sigma_x: 177.9 tauxy: 6.4 ------- OK!
pl_650.0x14.0 stf_L180.0x8.0+33.0x17.8 span: 1.0636 structure type: BOTTOM stf. type: L pressure side: p | sigma_y1: 128.6 sigma_y2: 128.6 sigma_x: 177.9 tauxy: 6.4 ------- OK!
pl_650.0x14.0 stf_L180.0x8.0+33.0x17.8 span: 1.0636 structure type: BOTTOM stf. type: L pressure side: p | sigma_y1: 128.6 sigma_y2: 128.6 sigma_x: 177.9 tauxy: 6.4 ------- OK!
pl_650.0x14.0 stf_L180.0x8.0+33.0x17.8 span: 1.0636 structure type: BOTTOM stf. type: L pressure side: p | sigma_y1: 128.6 sigma_y2: 128.6 sigma_x: 177.9 tauxy: 6.4 ------- OK!
pl_650.0x14.0 stf_L180.0x8.0+33.0x17.8 span: 1.0636 structure type: BOTTOM stf. type: L pressure side: p | sigma_y1: 128.6 sigma_y2: 128.6 sigma_x: 177.9 tauxy: 6.4 ------- OK!
pl_650.0x14.0 stf_L160.0x8.0+36.0x18.7 span: 1.0636 structure type: BOTTOM stf. type: L pressure side: p | sigma_y1: 128.6 sigma_y2: 128.6 sigma_x: 174.9 tauxy: 6.4 ------- OK!
pl_650.0x14.0 stf_L160.0x8.0+36.0x18.7 span: 1.0636 structure type: BOTTOM stf. type: L pressure side: p | sigma_y1: 128.6 sigma_y2: 128.6 sigma_x: 170.0 tauxy: 6.4 -END 1- OK!
pl_750.0x14.0 stf_L160.0x8.0+36.0x18.7 span: 1.0636 structure type: GENERAL_INTERNAL_WT stf. type: L pressure side: p | sigma_y1: 115.7 sigma_y2: 115.7 sigma_x: 144.9 tauxy: 6.4 START 2 OK!
pl_750.0x14.0 stf_L160.0x8.0+36.0x18.7 span: 1.0636 structure type: GENERAL_INTERNAL_WT stf. type: L pressure side: p | sigma_y1: 115.7 sigma_y2: 115.7 sigma_x: 144.9 tauxy: 6.4 ------- OK!
pl_750.0x14.0 stf_L160.0x8.0+36.0x18.7 span: 1.0636 structure type: GENERAL_INTERNAL_WT stf. type: L pressure side: p | sigma_y1: 115.7 sigma_y2: 115.7 sigma_x: 144.9 tauxy: 6.4 ------- OK!
pl_750.0x14.0 stf_L160.0x8.0+36.0x18.7 span: 1.0636 structure type: GENERAL_INTERNAL_WT stf. type: L pressure side: p | sigma_y1: 115.7 sigma_y2: 115.7 sigma_x: 144.9 tauxy: 6.4 ------- OK!
pl_750.0x14.0 stf_L160.0x8.0+36.0x18.7 span: 1.0636 structure type: GENERAL_INTERNAL_WT stf. type: L pressure side: p | sigma_y1: 115.7 sigma_y2: 115.7 sigma_x: 144.9 tauxy: 6.4 ------- OK!
pl_750.0x14.0 stf_L160.0x8.0+36.0x18.7 span: 1.0636 structure type: GENERAL_INTERNAL_WT stf. type: L pressure side: p | sigma_y1: 115.7 sigma_y2: 115.7 sigma_x: 144.9 tauxy: 6.4 ------- OK!
pl_750.0x14.0 stf_L160.0x8.0+36.0x18.7 span: 1.0636 structure type: GENERAL_INTERNAL_WT stf. type: L pressure side: p | sigma_y1: 115.7 sigma_y2: 115.7 sigma_x: 144.9 tauxy: 6.4 ------- OK!
pl_750.0x14.0 stf_L160.0x8.0+36.0x18.7 span: 1.0636 structure type: GENERAL_INTERNAL_WT stf. type: L pressure side: p | sigma_y1: 115.7 sigma_y2: 115.7 sigma_x: 144.9 tauxy: 6.4 ------- OK!
pl_750.0x14.0 stf_L160.0x8.0+36.0x18.7 span: 1.0636 structure type: GENERAL_INTERNAL_WT stf. type: L pressure side: p | sigma_y1: 115.7 sigma_y2: 115.7 sigma_x: 144.9 tauxy: 6.4 ------- OK!
pl_750.0x14.0 stf_L160.0x8.0+36.0x18.7 span: 1.0636 structure type: GENERAL_INTERNAL_WT stf. type: L pressure side: p | sigma_y1: 115.7 sigma_y2: 115.7 sigma_x: 144.9 tauxy: 6.4 ------- OK!
pl_750.0x14.0 stf_L160.0x8.0+36.0x18.7 span: 1.0636 structure type: GENERAL_INTERNAL_WT stf. type: L pressure side: p | sigma_y1: 115.7 sigma_y2: 115.7 sigma_x: 144.9 tauxy: 6.4 -END 2- OK!
Weight details for this solution:
Weight of main structure: ['1423.0', '1423.0', '1423.0', '1423.0', '1423.0', '1423.0', '1423.0', '1423.0', '1423.0', '1413.8', '1413.8', '1381.1', '1381.1', '1381.1', '1381.1', '1381.1', '1
Weight of frames:         ['4172.8', '4172.8', '4172.8', '4172.8', '4172.8', '4172.8', '4040.3', '4040.3', '4040.3', '4040.3']
Scales used on frames:    ['0.9', '0.9', '0.9', '0.9', '0.9', '0.9', '0.9', '0.9', '0.9', '0.9']
------------------------------------------------------------------------
```

Reporting

A pdf report can be created by clicking “Reporting - Generate PDF report”. The report will include all information for all lines. An example is seen next.



ANYstructure report generator

User: [redacted]

Time : Mon, 06 Jan 2020 09:13:50 +0000

ANYstructure

Compartments:

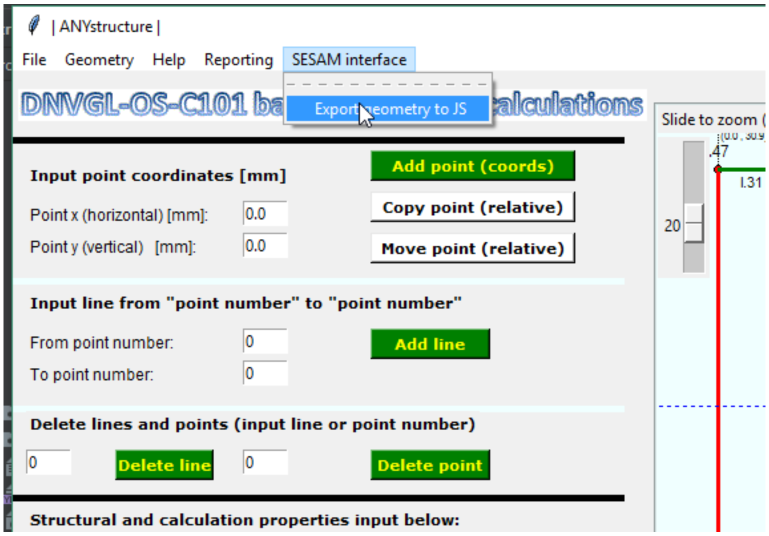
Compartments returned from search operation displayed below

Name: comp2, content:
Min. elevation: 2.5, Max. elevation: 30.9
Applied overpressure: 25000.0
(a_stat, a_dyn_loa, a_dyn_bal): (9.81, 3.0, 3.0)
Name: comp3, content:
Min. elevation: 2.5, Max. elevation: 30.900000000000002
Applied overpressure: 25000.0
(a_stat, a_dyn_loa, a_dyn_bal): (9.81, 3.0, 3.0)
Name: comp4, content:
Min. elevation: 0.0, Max. elevation: 30.900000000000002
Applied overpressure: 25000.0
(a_stat, a_dyn_loa, a_dyn_bal): (9.81, 3.0, 3.0)
Name: comp5, content:
Min. elevation: 0.0, Max. elevation: 2.5
Applied overpressure: 25000.0
(a_stat, a_dyn_loa, a_dyn_bal): (9.81, 3.0, 3.0)

*********** line1 ***********
Plate thickness: 14.0 [mm]   Stiffener spacing: 700.0 [mm]   Span: 2.5 [m]
Stiffener: 250.0x18.0 + 0.0x0.0
Fixation paramters: kps: = 1.0 kpp = 1.0, Bending moment factors km1/km2/km3 (support/field/support) = 12/24/12
Defined stresses [MPa]: sigma_x = 40.0 sigma_y1 = 40.0 sigma_y2 = 40.0 tau_xy = 5.0
ULS max pressure for line: 60.0 [kPa]   Pressure applied at: plate side
Fatigue pressure: No pressures defined
Section modulus: 360000 [mm3] Min. section modulus: 80351 [mm3] -> OK
Min plate thickness: 4.88 [mm] -> OK
Shear area: 4751 [mm2]   Min shear area: 296 [mm2] -> OK
Highest buckling utilization: 0.41 -> OK
No fatigue results
Utilization percentage (highest calculated): 41%
*********** line10 ***********
Plate thickness: 18.0 [mm]   Stiffener spacing: 750.0 [mm]   Span: 3.8 [m]
Stiffener: 350.0x12.0 + 150.0x20.0
Fixation paramters: kps: = 1.0 kpp = 1.0, Bending moment factors km1/km2/km3 (support/field/support) = 12/24/12
Defined stresses [MPa]: sigma_x = 100.0 sigma_y1 = 100.0 sigma_y2 = 100.0 tau_xy = 5.0
ULS max pressure for line: 510.0 [kPa]   Pressure applied at: plate side
Fatigue pressure [Pa]: p_int: loaded/ballast/part = 0/0/0 p_ext: loaded/ballast/part = 0/40000.0/0
Section modulus: 1470000 [mm3] Min. section modulus: 2073943 [mm3] -> NOT OK
Min plate thickness: 15.76 [mm] -> OK
Shear area: 4656 [mm2]   Min shear area: 4129 [mm2] -> OK
Highest buckling utilization: 1.39 -> NOT OK
Fatigue (plate/stiffeners) utilization: 0.06 * DFF(2.0) = 0.12 (SN-curve = Ec)
Utilization percentage (highest calculated): 141%
*********** line11 ***********
Plate thickness: 18.0 [mm]   Stiffener spacing: 750.0 [mm]   Span: 4.0 [m]
Stiffener: 350.0x12.0 + 150.0x20.0
Fixation paramters: kps: = 1.0 kpp = 1.0, Bending moment factors km1/km2/km3 (support/field/support) = 12/24/12
Defined stresses [MPa]: sigma_x = 100.0 sigma_y1 = 100.0 sigma_y2 = 100.0 tau_xy = 5.0
ULS max pressure for line: 550.0 [kPa]   Pressure applied at: plate side
Fatigue pressure [Pa]: p_int: loaded/ballast/part = 0/0/0 p_ext: loaded/ballast/part = 0/40000.0/0
Section modulus: 1470000 [mm3] Min. section modulus: 2465181 [mm3] -> NOT OK
Min plate thickness: 16.32 [mm] -> OK
Shear area: 4656 [mm2]   Min shear area: 4663 [mm2] -> NOT OK
Highest buckling utilization: 1.63 -> NOT OK
Fatigue (plate/stiffeners) utilization: 0.06 * DFF(2.0) = 0.12 (SN-curve = Ec)
Utilization percentage (highest calculated): 167%
*********** line12 ***********
Plate thickness: 18.0 [mm]   Stiffener spacing: 750.0 [mm]   Span: 3.9051 [m]
Stiffener: 350.0x12.0 + 150.0x20.0
Fixation paramters: kps: = 1.0 kpp = 1.0, Bending moment factors km1/km2/km3 (support/field/support) = 12/24/12
Defined stresses [MPa]: sigma_x = 100.0 sigma_y1 = 100.0 sigma_y2 = 100.0 tau_xy = 5.0
ULS max pressure for line: 590.0 [kPa]   Pressure applied at: plate side
Fatigue pressure [Pa]: p_int: loaded/ballast/part = 0/0/0 p_ext: loaded/ballast/part = 0/40000.0/0
Section modulus: 1470000 [mm3] Min. section modulus: 2516366 [mm3] -> NOT OK
Min plate thickness: 16.89 [mm] -> OK
Shear area: 4656 [mm2]   Min shear area: 4875 [mm2] -> NOT OK
Highest buckling utilization: 1.64 -> NOT OK
Fatigue (plate/stiffeners) utilization: 0.06 * DFF(2.0) = 0.12 (SN-curve = Ec)
Utilization percentage (highest calculated): 171%
*********** line13 ***********
Plate thickness: 18.0 [mm]   Stiffener spacing: 775.0 [mm]   Span: 4.0 [m]
Stiffener: 375.0x12.0 + 150.0x18.0
Fixation paramters: kps: = 1.0 kpp = 1.0, Bending moment factors km1/km2/km3 (support/field/support) = 12/24/12
Defined stresses [MPa]: sigma_x = 90.0 sigma_y1 = 90.0 sigma_y2 = 90.0 tau_xy = 5.0
ULS max pressure for line: 310.0 [kPa]   Pressure applied at: plate side
Fatigue pressure: No pressures defined
Section modulus: 1500000 [mm3] Min. section modulus: 1394615 [mm3] -> OK
Min plate thickness: 12.48 [mm] -> OK
Shear area: 4932 [mm2]   Min shear area: 2725 [mm2] -> OK
Highest buckling utilization: 1.06 -> NOT OK
No fatigue results
Utilization percentage (highest calculated): 106%

Export to JS

ANYstructure can export points, lines and section properties to SESAM GeniE. A dialog will request a location to save the JS file. After that you can read the js file into GeniE.



The result is illustrated below: